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FINAL REPORT

SPACE SHUTTLE MAIN ENGINE STRUCTURAL ANALYSIS AND DATA REDUCTION/EVALUATION

VOLUME 6: PRIMARY NOZZLE DIFFUSER ANALYSIS

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FOREWORD

This volume of the final report summarizes the analysis performed on the Primary Nozzle Diffuser located on the Space Shuttle Main Engine. Static stress analysis was performed by Michael J. Foley, P.E., in the Structures & Mechanics Section of the Lockheed-Huntsville Engineering Center under Contract NAS8-37282.

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1. INTRODUCTION AND OVERVIEW

The Primary Nozzle Diffuser routes fuel from the main fuel valve on the SSME to the nozzle coolant inlet manifold, main combustion chamber coolant inlet manifold, chamber coolant valve, and the augmented spark igniters. The diffuser also includes the fuel system purge check valve connection. Figure 1 shows the location of the diffuser with respect to the SSME nozzle.

A static stress analysis was performed on the diffuser because no detailed analysis has been done on this part in the past. Structural concerns were in the area of the welds because approximately 10% are in areas inaccessible by x-ray testing devices. Flow dynamics and thermodynamics were not included in the analysis load case. Constant internal pressure at maximum SSME power was used instead.

A three-dimensional, finite element model was generated using ANSYS version 4.3A on Lockheed's VAX 11/785 computer to perform the stress computations. IDEAS Supertab on a Sun 3/60 computer was used to create the finite element model. Rocketdyne drawing number RS009156 was used for the model interpretation. The flight diffuser is denoted as -101.

A description of the model, boundary conditions/load case, material properties, structural analysis/results, and a summary are included for documentation.

2. MODEL DESCRIPTION

An ANSYS finite element model was made for the primary nozzle diffuser using Supertab for the model generation. The model consists of 1922 nodes and 1873 elements. The model is constructed using quadrilateral shell elements except for two triangular shell elements that were used for special geometry condi'ions. Both element types are capable of bending as well as membrane behavior. Figure 2 shows an isometric, hidden line plot of the undeformed geometry. From the figure, the modeled attachment bracket, inlet flange, and outlet tubes can be identified. Table 1 lists the model component groups, element numbering ranges, radii, element thicknesses, and property numbers. Although the table lists each outlet cylinder and the sphere as having a constant element thickness, some elements around the interfaces are thicker to represent the fillet areas on the hardware. A unique property number was used with each element thickness, but the entire model consists of only one material type.

The diffuser assembly has two bosses and numerous fillets which were not modeled because of the extensive detail required. Various wall thicknesses resulting from these bosses, fillets, and elliptical tangents could only be modeled with dictinct thickness changes over the length of the diffuser and around the sphere and outlet cylinders. The outlet for the augmented spark igniters and the fuel system purge opening were not modeled explicitly.

Table 1 SSME DIFFUSER MODEL DATA

	A	B	C	D	E	F	G	H	I	J
1	GROUP	ITEM	SUBAREA	1ST ELEM	NO ELEM	LAST ELEM	RADIUS	THICKNESS	PROP	S (ksi)
2										
3	1	CYL1	32	1	64	64	1.2275	0.135	1	64
4			5	65	42	106				
5			4	107	34	140				
6			3	141	32	172				
7			1	173	26	198				
8	2	CYL2	10	199	8	206	0.935	0.105	2	32
9			9	207	29	235				
10			8	236	34	269				
11			7	270	19	288				
12			6	289	19	307				
13	3	CYL3	14	308	21	328	0.75	0.135	1	39
14			13	329	9	337				
15			12	338	13	350				
16			11	351	29	379				
17	4	CYL4	20	380	14	393	0.75	0.135	1	39
18			19	394	11	404				
19			18	405	6	410				
20			17	411	4	414				
21			16	415	2	416				
22			15	417	2	418				
23	5	CYL5	25	419	4	422	0.75	0.135	1	39
24			24	423	22	444				
25			23	445	15	459				
26			22	460	10	469				
27			21	470	28	497				
28	6	SPHERE	1024	498	7	504	2.32	0.25	3	32
29			1023	505	4	508				
30			1022	509	4	512				
31			1021	513	7	519				
32			1020	520	6	525				
33			1019	526	6	531				
34			1018	532	1	532				
35			38	533	17	549				
36			37	550	83	632				
37			36	633	66	698				
38			35	699	26	724				
39			34	725	29	753				
40			33	754	40	793				
41			31	794	63	856				
42			30	857	2	858				
43	7	FLANGE	1025	859	52	910		1.12	4	0
44			1017	911	52	962				
45			1016	963	52	1014				
46			1015	1015	52	1066				
47	8	BRACKET	1006	1067	48	1114		0.125	5	0
48			1005	1115	51	1165				
49			1004	1166	63	1228				
50			1003	1229	63	1291				
51	9	DIFFUSER	1031	1292	64	1355	2.206	0.4	7	39
52			1030	1356	64	1419				
53			1029	1420	20	1439				
54			1028	1440	22	1461				
55			1027	1462	46	1507				
56			1026	1508	46	1553				
57			1010	1554	79	1632	1.3725	0.18	8	60
58			1009	1633	80	1712				
59			1008	1713	79	1791				
60			1007	1792	80	1871				
61	10	TRIANGLES	1002	1872	1	1872		0.125	5	0
62			1001	1873	1	1873				

3. BOUNDARY CONDITIONS/LOAD CASE

The model was constrained at the inlet flange, the attach bracket, and the outlet cylinders. The inlet flange constraints were imposed at a radius equal to the radius of the 14 attaching bolts. The diffuser was also constrained by the attach bracket which connects the component to the coolant outlet manifold. The bracket was modeled to an adequate length to simulate the hardware attachment stiffness, and full constraints were added. Finally, all five outlet tubes were constrained at the weld interfaces. All six (three translational and three rotational) degrees of freedom were fixed for all constraints.

Bernoulli's fluid flow equation,

$$\frac{p}{\rho} + gz + \frac{V^2}{2} = \text{constant}$$

for steady state, incompressible, streamlined flow, has been greatly simplified by ignoring the fluid weight, gz, and the flow rate, $V^2/2$. The only load case analyzed was for an internal pressure of 6980 psi. This value was obtained from the structural audit of the component dated 23 May 1986 and was applied on all internal surfaces. The flange and bracket assemblies were not loaded by fuel pressure. This pressure was higher than the fuel pump discharge pressure at Full Power Level and therefore the analysis was considered conservative.

Thermal loads were ignored because no thermal gradients exist in the diffuser. The thermal environment for the component is -350 °F, which is the fuel temperature.

4. MATERIAL PROPERTIES

The primary nozzle diffuser is an Inconel 718 forging. Table 2 lists the material properties used in the analysis.

Table 2 MATERIAL PROPERTIES

Inconel 718 Forging	
Yield stress, σ_y	150 ksi
Ultimate stress, σ_u	180 ksi
Young's modulus, E	30,000 ksi
Poisson's ratio, ν	0.291
Density, ρ	0.7254E-3 lb-s^2/in.
Temperature, α*	0.2006E-5 in/in/°F

*Thermal effects were neglected.

Fatigue analysis was not performed, so signal-to-noise curves for this material were not required.

5. STRUCTURAL ANALYSIS/RESULTS

The ANSYS finite element code was used to determine the stress distribution for the model under the static pressure load. A failure criterion of maximum yield stress was used in this analysis to compute a minimum margin of safety for the component.

Principal stress contour plots on the exaggerated deformed diffuser model are shown in Figures 3 through 11. For the five cylindrical output tubes and the main diffuser cylinder, the ANSYS calculated maximum stress away from the end conditions closely follows that computed using the classical analysis value, pr/t. Table 3 lists the classical maximum stress, the ANSYS computed stress away from end conditions, and the margin of safety for the cylindrical diffuser parts. The ANSYS values were determined graphically from Figures 3 through 7 and Figure 11.

Table 3 DIFFUSER STRESSES

Model Part	*Radius, r*	*Thickness, t*	σ, *classical*	σ, *ANSYS*	*M.S.* *
Cylinder 1	1.2275 in.	0.135 in.	63.5 ksi	67.1 ksi	1.2
Cylinder 2	0.935	0.105	62.2	66.8	1.2
Cylinder 3	0.75	0.135	38.8	34.8	3.3
Cylinder 4	0.75	0.135	38.8	33.4	3.5
Cylinder 5	0.75	0.135	38.8	37.2	3.0
Diffuser (1)	2.206	0.40	38.5	38.9	2.9
Diffuser (2)	1.3725	0.16	59.9	60.8	1.5
p = 6980 psi constant		*Margin of Safety (yield) = (150 ksi/σ_{ansys}) - 1			

The maximum stress values for the outlet cylinders are at the cylinder/sphere or cylinder/cylinder interfaces. Table 4 lists each outlet cylinder and the maximum stress in the cylinder. Again, these values were determined using Figures 3 through 7.

Table 4 MAXIMUM CYLINDER STRESSES

CYLINDER NO.	MAX STRESS
1	84.8 ksi
2	81.9
3	59.1
4	62.8
5	88.1

The highest stressed elements are in the region of the fillets around the interfaces. The thicknesses used here are thought to be conservative in view of the geometry shown on the drawings.

The classical solution for the maximum principal stress in a sphere under internal pressure is pr/2t. For the diffuser sphere, this value is

$$\sigma_{sphere} = \frac{6.98 \text{ ksi } (2.32 \text{ in.})}{2\ (0.25 \text{ in.})} = 32.4 \text{ ksi}$$

The typical stress found in the sphere model is 47.6 ksi, which is higher than the classical solution. This is due to the outlet tube openings which require the surrounding sphere regions to carry a higher load. The maximum principal stress in the sphere is 92.6 ksi and occurs between cylinders 2 and 5.

The flange, the bracket, and the diffuser section are not critically stressed. The highest flange stress was located where the diffuser tube meets the flange, but the stress there was very low (1.3 ksi). The attach bracket is stressed highest at the diffuser tube connection. From Figure 10, it is found that this stress is 36.6 ksi. The conical diffuser section was modeled with two thicknesses. The diffuser plot, Figure 11, shows the division plane of these sections. The maximum principal stress is found to be in the thinner section. A hoop stress of 82.7 ksi occurs in this region.

6. SUMMARY

Under pressure loading, the diffuser exhibits highest stresses at the interface between the sphere and the outlet tubes. Close study of these areas shows that a conservative element thickness value has been used. Table 5 lists all the sections of the primary diffuser model and the minimum margins of safety. All margins of safety were positive.

Table 5 MARGINS OF SAFETY

Model Part	*Maximum Stress*	*M.S.**
Cylinder 1	84.8 ksi	0.8
Cylinder 2	81.9	0.8
Cylinder 3	59.1	1.5
Cylinder 4	62.8	1.4
Cylinder 5	88.1	0.7
Sphere	92.6	0.6
Flange	1.3	high
Bracket	36.6	3.1
Diffuser (1)	82.7	0.8
Diffuser (2)	65.2	1.3

* M.S.(yield)=(150ksi/σ_{max}) - 1

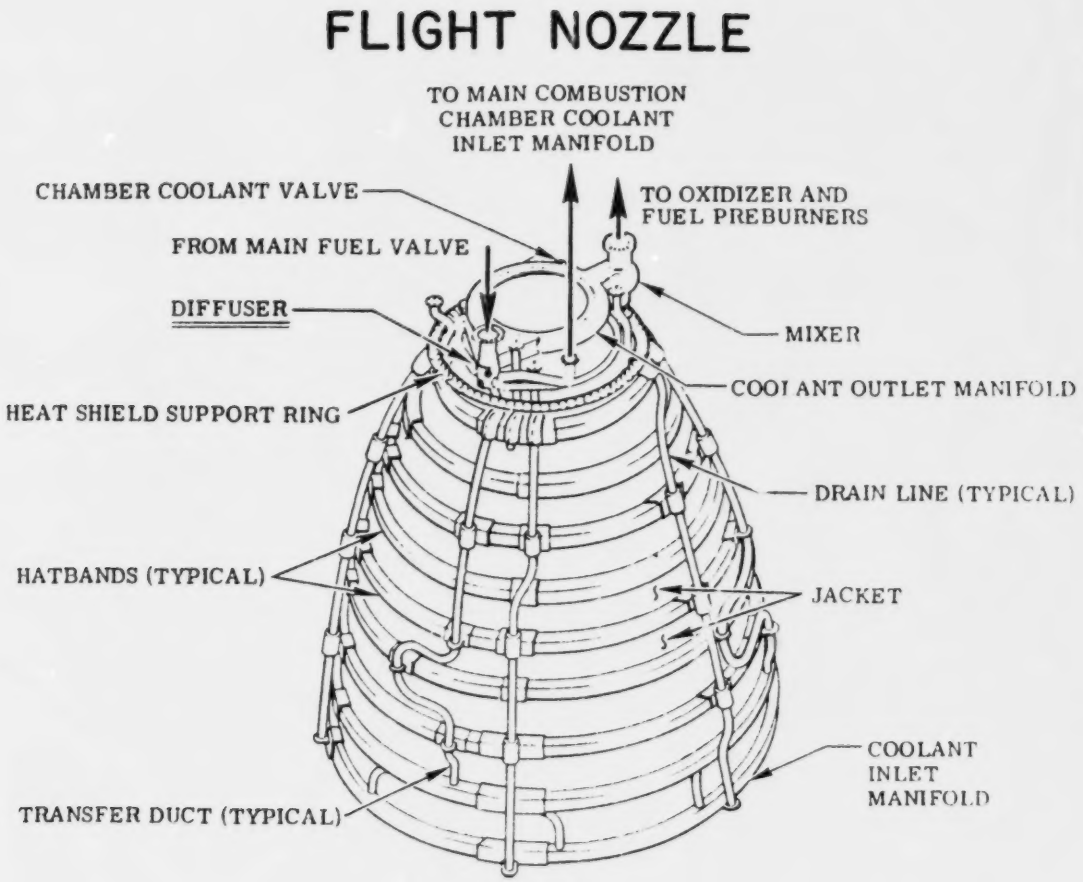

Figure 1 SSME Nozzle

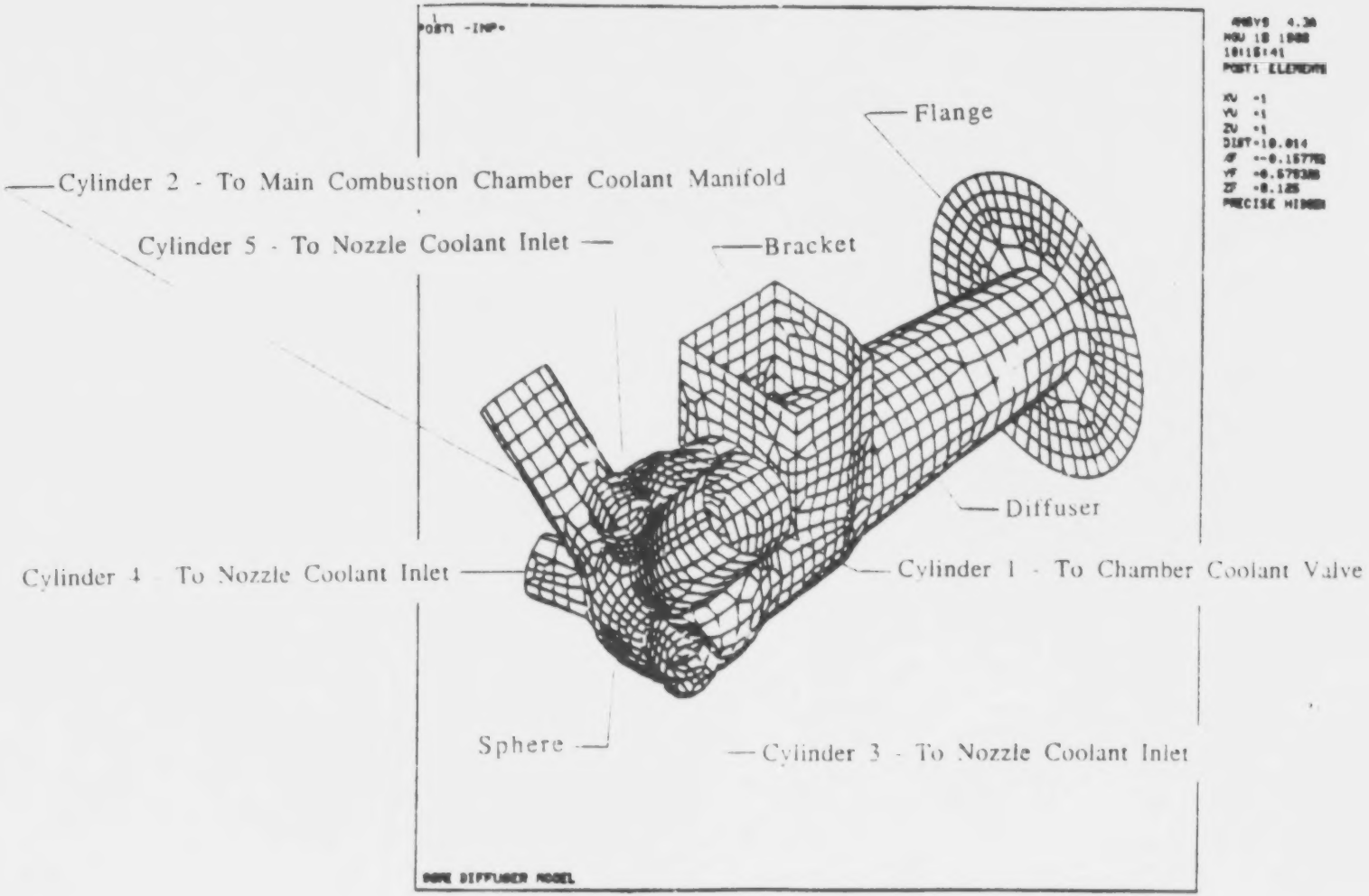
Flange
Cylinder 2 - To Main Combustion Chamber Coolant Manifold
Cylinder 5 - To Nozzle Coolant Inlet
Bracket
Diffuser
Cylinder 4 - To Nozzle Coolant Inlet
Cylinder 1 - To Chamber Coolant Valve
Sphere
Cylinder 3 - To Nozzle Coolant Inlet

Figure 2 SSME Diffuser Model

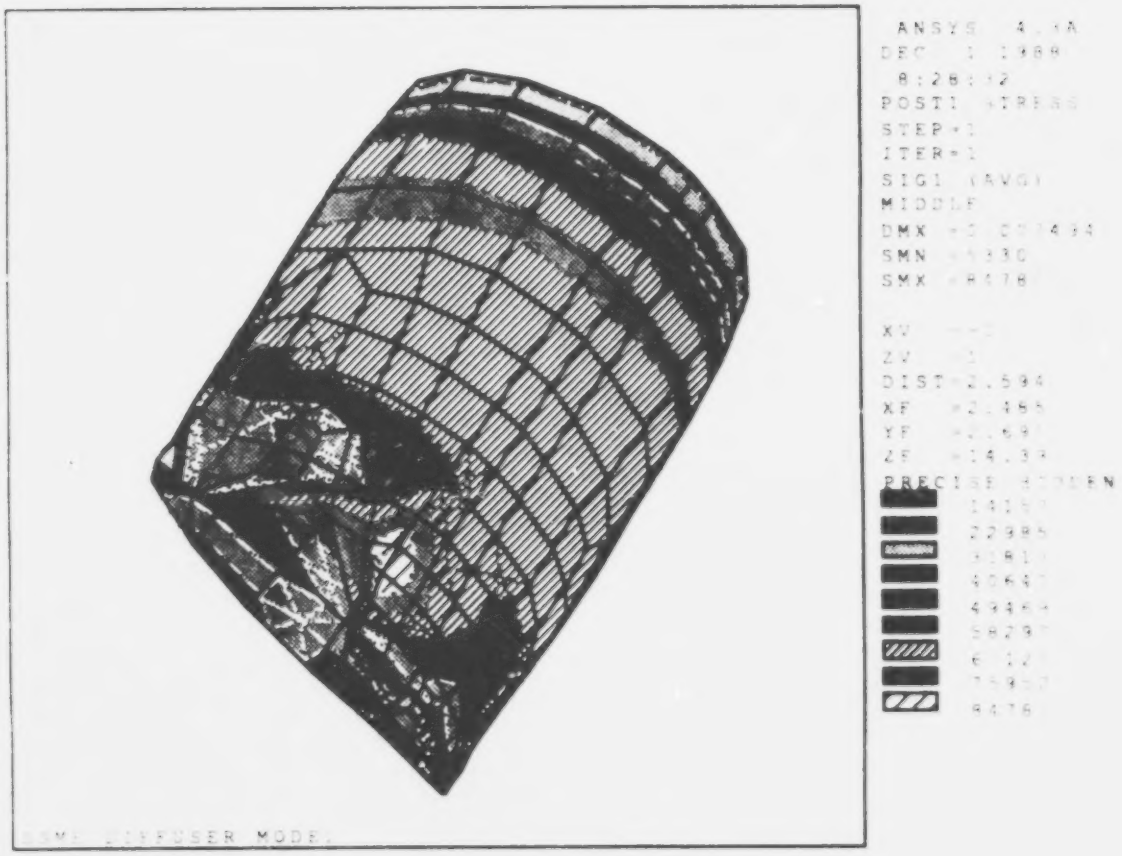

Figure 3 Cylinder 1 - To Chamber Coolant Valve

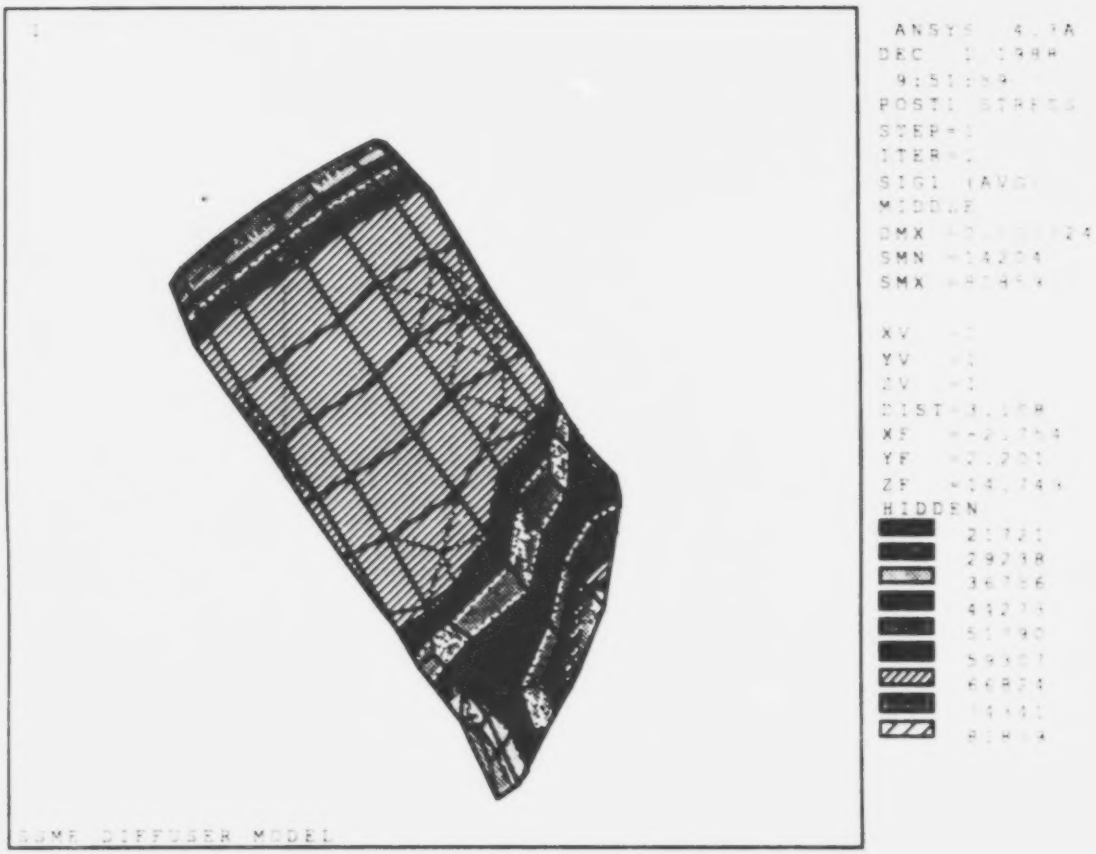

Figure 4 Cylinder 2 - To Main Combustion Chamber Coolant Manifold

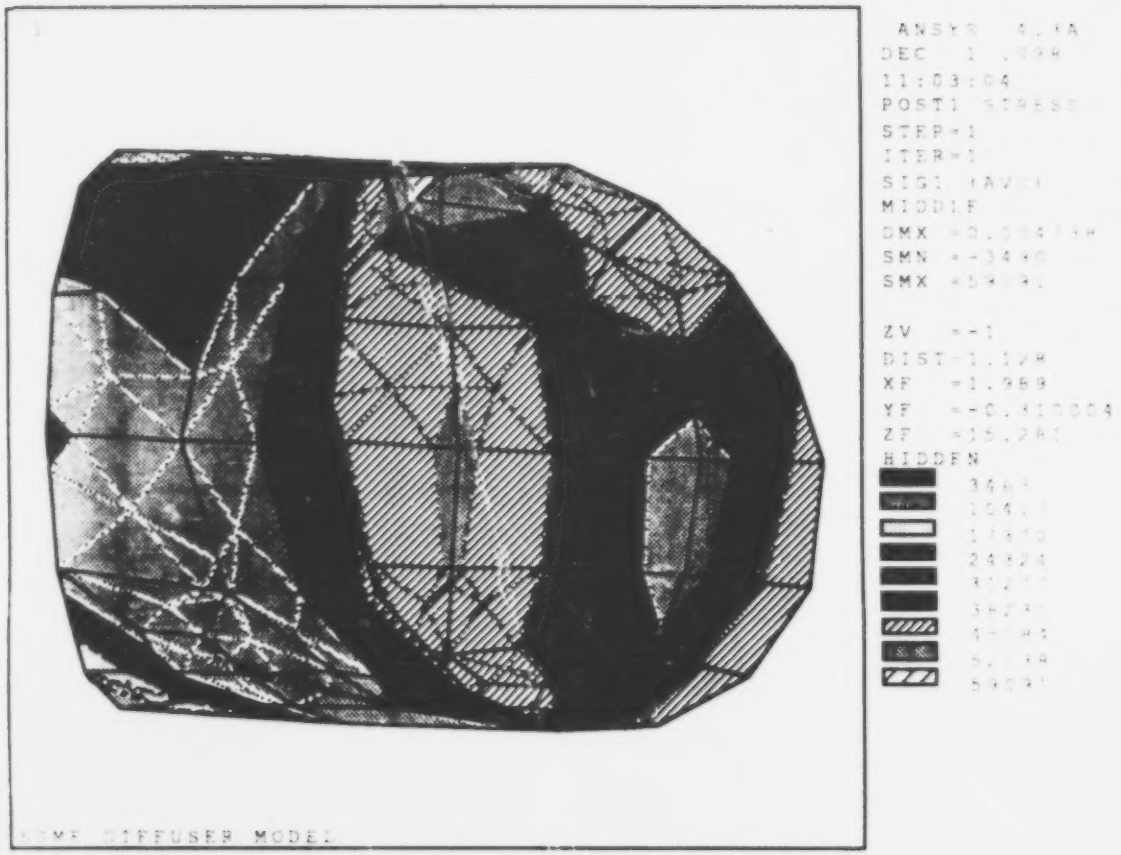

Figure 5 Cylinder 3 - To Nozzle Coolant Inlet

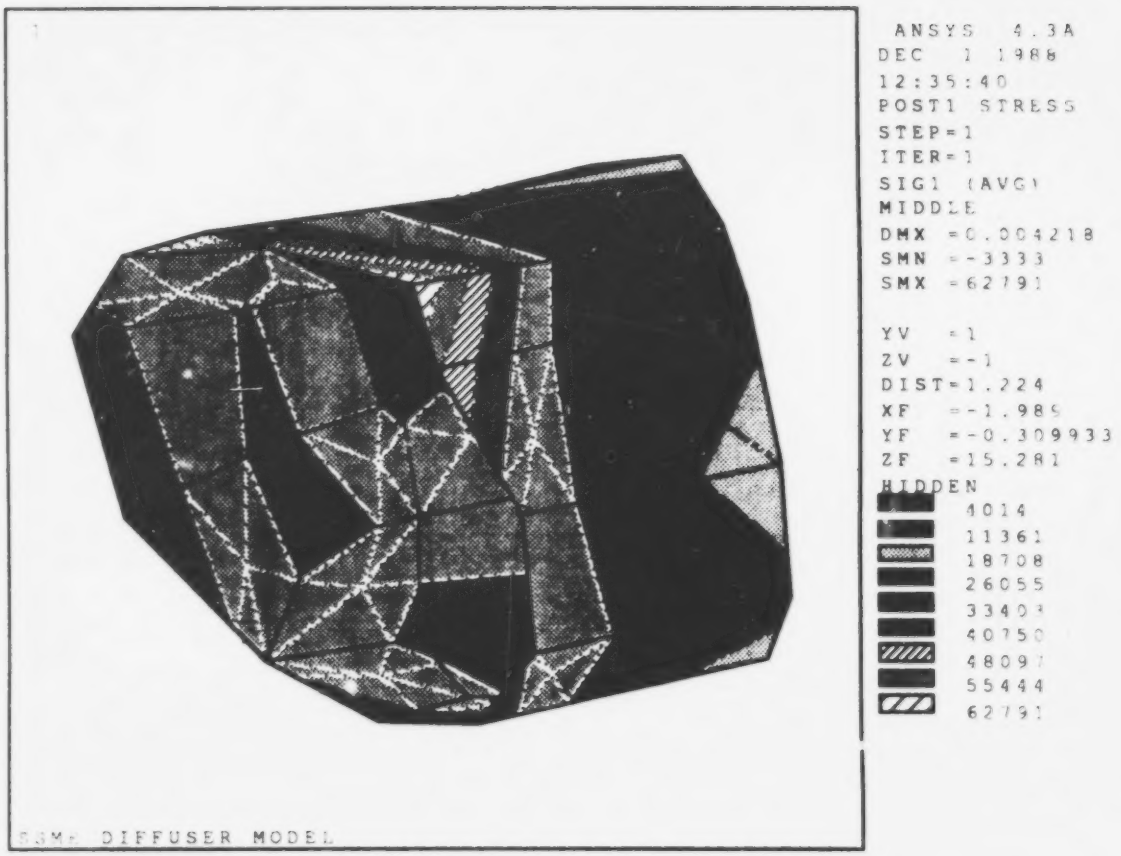

Figure 6 Cylinder 4 - To Nozzle Coolant Inlet

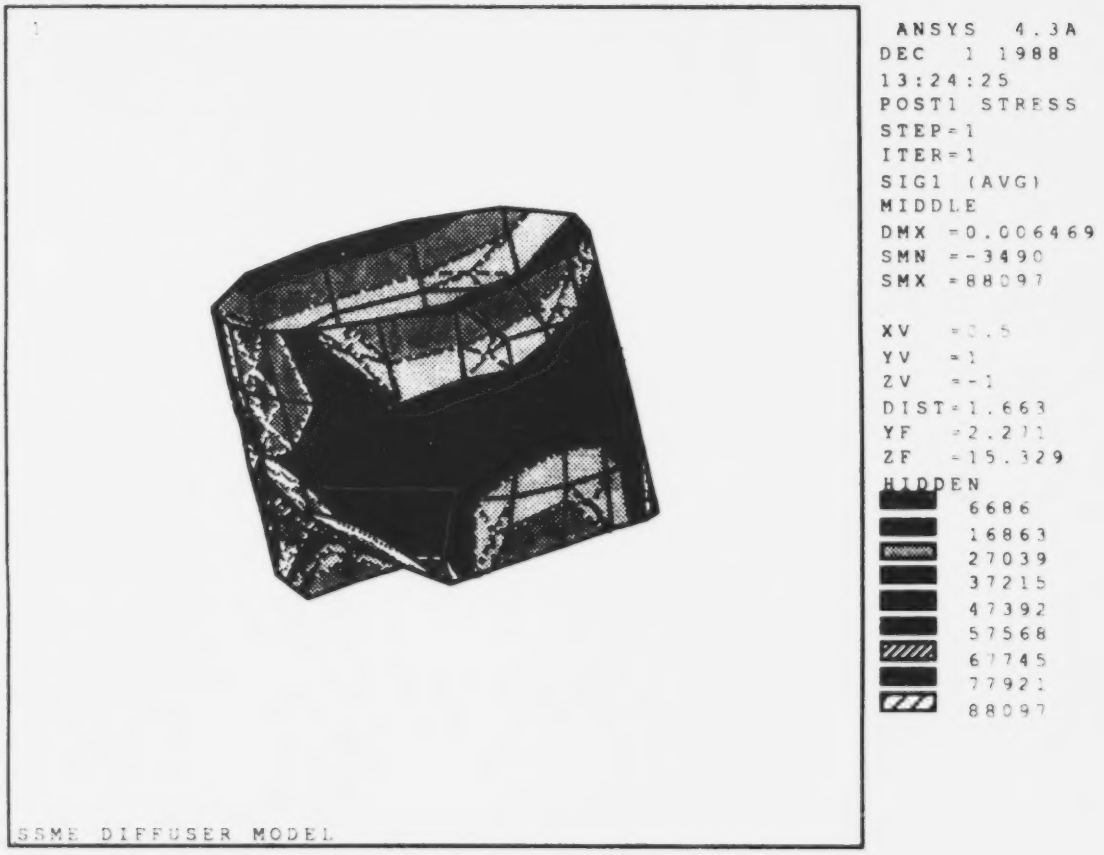

Figure 7 Cylinder 5 - To Nozzle Coolant Inlet

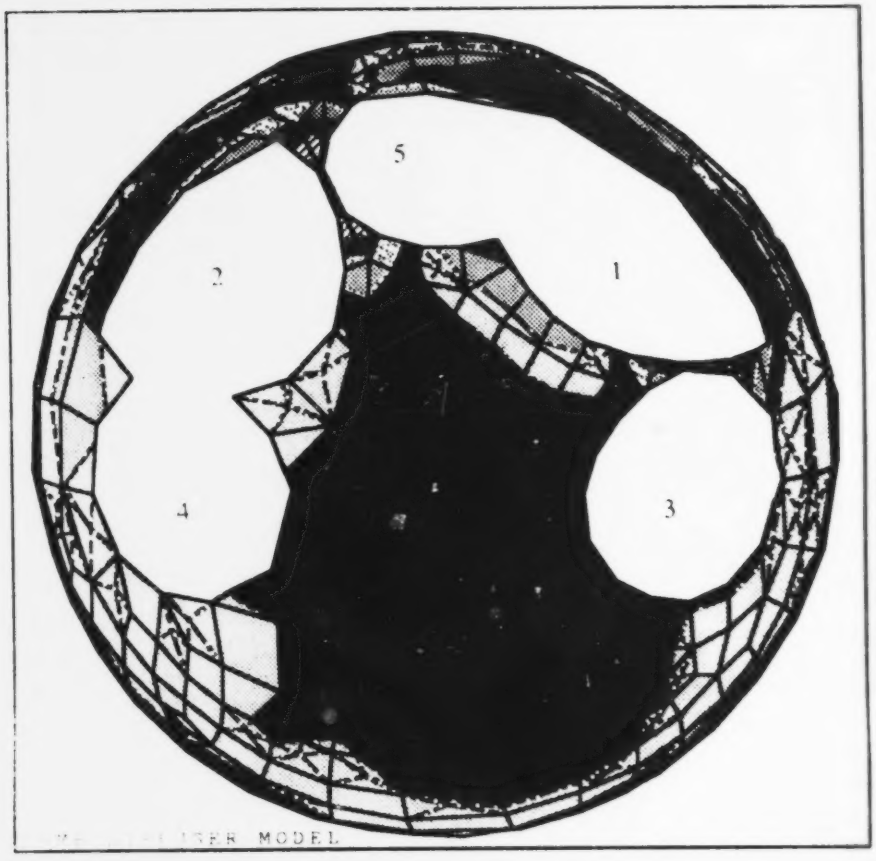

Figure 8 Sphere

Figure 9 Flange

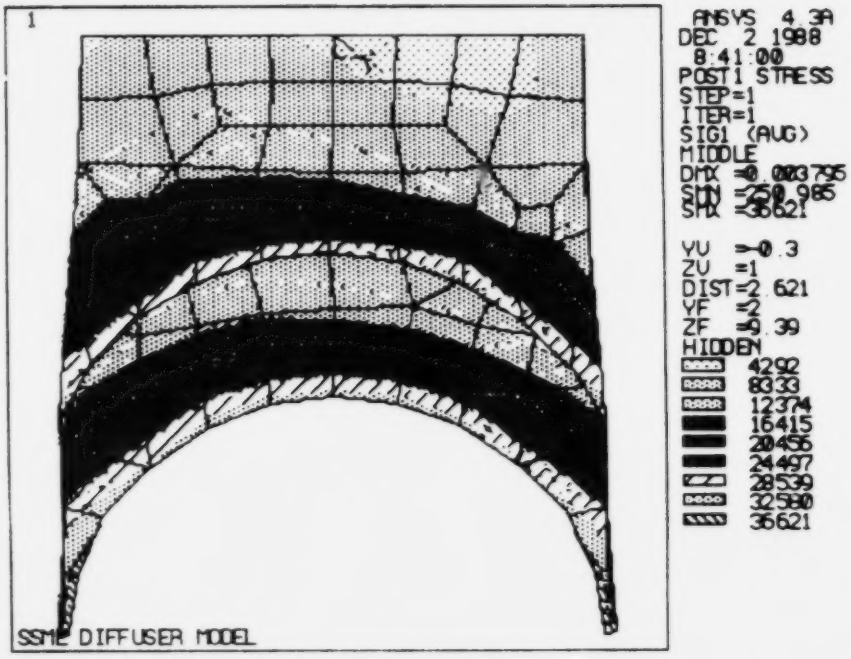

Figure 10 Bracket

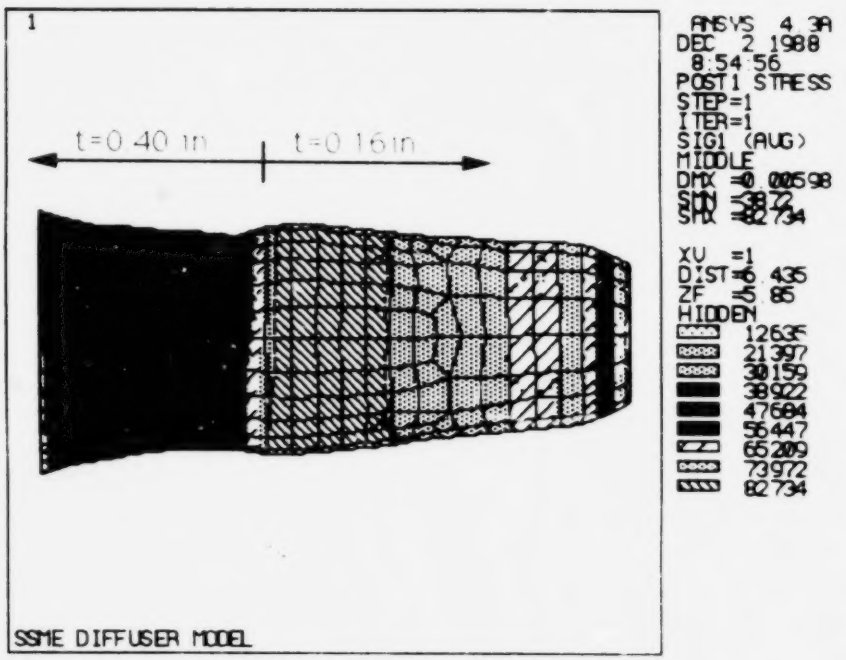

Figure 11 Diffuser

Appendix A
MODEL LISTING

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